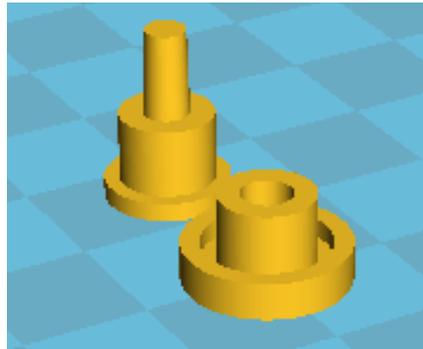


by Fritz Ruoss

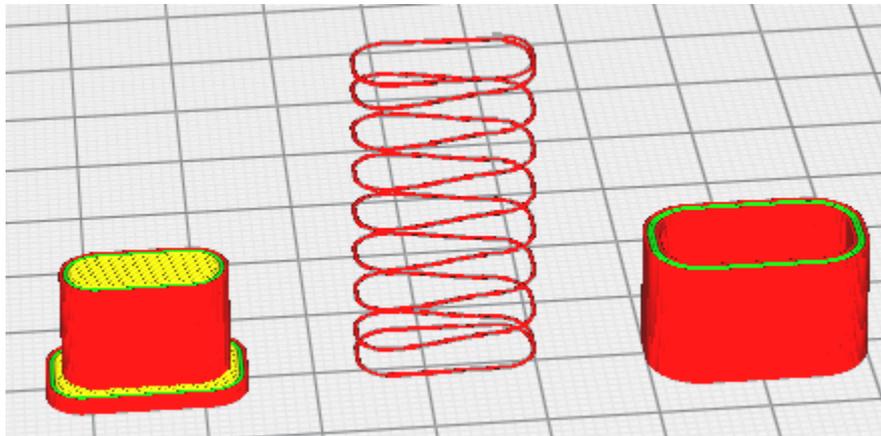
FED1+, FED5: Produce spring utilities mandrel and bore with 3D printer

Shaft and hub with mandrel and bore, generated as STL file and produced with 3D printer, can be used for a test assembly of the spring and compression up to spring length L2.

**FED17 - Print mandrel and sleeve for magazine spring**

Mandrel and bore for magazine springs can be generated as an STL file and produced with a 3D printer now.

You can also enter the setting length under “Edit \ Production drawing” in FED17 now.

**FED1..17: Warnings for fatigue strength diagram for hot formed springs**

In EN 13906, there is only one fatigue strength diagram for hot coiled springs: for hot rolled steels according to EN 10089 with ground or peeled surface, shot blasted. Unlike cold-formed springs, the spring is fatigue strength safe in 2 million cycles, not 10 million like cold-formed springs.

Conversely, a shorter life is calculated from dynamic shear stress: If the allowable variation of stress for fatigue strength is slightly exceeded, then the life is not a little less than 10 million load cycles, but less than 2 million cycles.

The fatigue 2E6 load cycling diagram does not automatically apply to hot formed springs and / or EN10089 spring bars, it must be configured under "Edit \ Calculation Method". There are now 2 new alerts as hint for possibly inappropriate setting:

Warning: EN10089 fatigue 2E6 if hot formed or material EN10089, but fatigue diagram 1E7.

Warning: Fatigue 1E7 > <2E6? if cold-formed spring, but fatigue strength 2E6 set.

SR1/SR1+: Configure default material database

SR1+ calculation base

calculation base FM, MA
 VDI 2230 : 1986
 VDI 2230-1:2015

dPzu (80) VDI 2230-1:2015

Elasticity
 deformation sleeve (VDI 2230-1986)
 deformation cone (VDI 2230-1:2015)

p max
 deformation sleeve

TTJ -> TBJ (phiD, dw nut)
 D'A max = 10 dw

washer dwa=dw+1.6hs

creep at FV min

thread length engaged to Dose

calc. min. thread length engag. for FSmax (=FMzul+FSA)

Tolerances for friction coefficients ?

tolerances d2, d3 for FM, MA ? nom. dim. (d2=d2nom, d3=d3nom)

Multi-bolted joint (FA,FQ,FKR = f (MV) ?
No Flange

calculation FA (Mb) flange
 Dose, VDI2230-2 (34)
 VDI2230-2 (43): FAmax=4*Mb/(ns*dt)

tightening angle incl. torsion bolt ?

TTJ: thread engagement mgeo and mtr reduced by bolt length tolerance

Use approximation to reduce calculation time MA = f (FM)

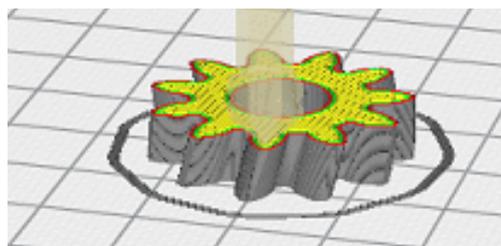
Units metric/imperial metric (mm, N, MPa, Nmm, °C)

Default Mat mat_p_1.dbf
pressung.dbf
mat_p_1.dbf
mat_p_2.dbf

OK Cancel Help Text Calc

When selecting the materials for clamping plates and nuts, you can choose between the database files `pressung.dbf`, `mat_p_1.dbf` and `mat_p_2.dbf`. The default setting can now be configured under "Edit \ Calculation Method" (Default Mat). If you want to use a database with your own material data, the best way is to use `mat_p_1.dbf`. This contains material data from VDI 2230: 2003, which you no longer need. If you have not yet used `mat_p_1.dbf` for previous calculations, you can delete and replace the existing records, otherwise you may append your own data to the bottom. `Mat_p_2.dbf` contains the materials from VDI 2230:2015, and `pressung.dbf` contains all old and new material data.

ZAR1+, ZAR5, ZAR6, ZAR7, ZAR8: Helical gears by means of 3D printer



Up to now, only straight-toothed gears could be output as STL files for 3D printer production. This is now also possible for helical teeth. The helix is represented as a staircase function. Minimal stair width is the smallest possible layer thickness of the 3D printer. Suitable as an illustrative and functioning model, but rather unusable for practical use.

ZAR3+: Strength Calculation according to DIN 3996:2012-09

The strength of worm gears was previously calculated according to DIN 3996:1998-09. Now, the newer edition of 2012 has been integrated. ZAR3 + can now calculate strength and efficiency according to 3 methods: according to Niemann, according to DIN 3996: 1998 and according to DIN 3996: 2012. There were some changes on input:

- Polyalphaolefins were added to the lubricants
- Lubricant viscosity must now be entered for 40 ° C and 100 ° C, not for 50 ° C
- Enter the number of sealing rings for power loss PD
- Select the wear limit: $0.3 m_x \cdot \cos(\gamma_m)$ or pointed tooth

The screenshot shows the ZAR3+ software interface with the following input fields and values:

- Calculation acc. DIN 3996 ?
- lubrication fluid: Polyglycol (EO:PO = 0:1)
- splash lubrication
- Bearing: fix bearing, fix/loose bearing
- gear wheel temperature thetaM: 77,1 C
- dynamic oil viscosity eta OM: 0,064 Ns/m²
- material lubrication coefficient WML: 1,75
- application factor KA: 1
- Min. Life expect. LH: 25000 h
- wear limit: $\Delta W / \lim_n = 0.3 \cdot m_x \cdot \cos(\gamma_m)$
- Tooth friction value μ_z : 0,028 (Niemann)

Some help pictures had to be supplemented and updated because of changed characteristics in DIN 3996: 2012.

ZAR3+ Worm Gear Design V 10.2 #0152 JAHWA Elec... File Edit View CAD STL Database Document OLE Help

Worm: 16MnCr5	material lubrication coefficient WML to DIN 3996:1998		
Worm wheel material	Mineral Oil	Polyglycol EO:PO = 0:1	Polyglycol EO:PO = 1:1
GZ-CuSn12Ni	1.0	1.2	2.3
GZ-CuSn12	1.6	1.5	-
GZ-CuAl10Ni	2.5	-	-

Worm: 16MnCr5	material lubrication coefficient WML to DIN 3996:2012		
Worm wheel material	Mineral Oil	Polyalphaolefin	Polyglycol
CuSn12-C-GZ	1.6	1.6	2.25
CuSn12Ni2-C-GZ	1.0	1.0	1.75
CuSn12Ni2-C-GC	4.1	4.1	4.1
CuAl10Fe5Ni5-C-GZ	1	1	-
EN-GJS-400-15	1	1	1
EN-GJL-250	1	1	1

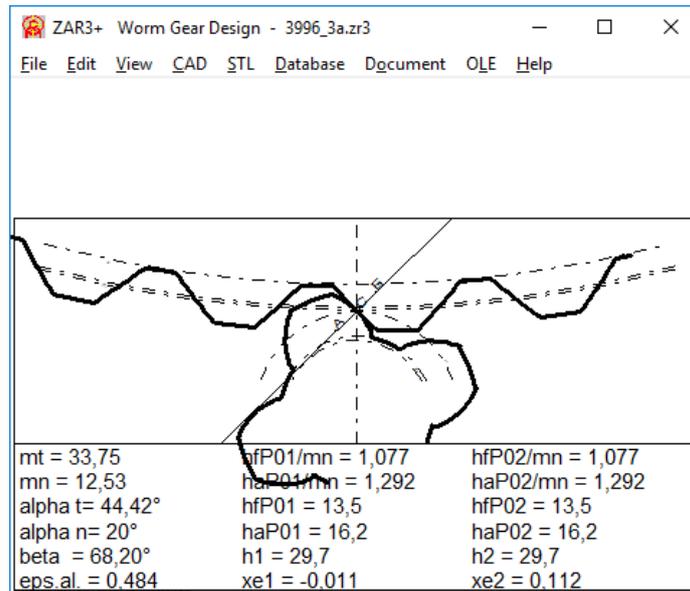
Z3-E-103 Source: DIN 3996 Z3-E-103
ZAR3 Material-Lubrication-Coefficient WML FB_05/13

Material coefficient YW	3996:1998	3996:2012
Worm wheel material	YW	YW
GZ-CuSn12 (CuSn12-C-GZ)	1.0	1.0
GZ-CuSn12Ni (CuSn12Ni2-C-GZ / GC)	0.95	0.95
GZ-CuAl10Ni (CuAl10Fe5Ni5-C-GZ)	1.1	1.1
EN-GJS-400-15 (GGC-40)	1.3	1.0
EN-GJL-250 (GG-25)	1.4	1.05

Shear Fatigue Strength tauFlimT		
worm gear material according to DIN	shear fatigue strength tauFlimT in N/mm²	reduced shear fatigue strength tauFlimT in N/mm²
GZ-CuSn12 (CuSn12-C-GZ)	92	82
GZ-CuSn12Ni	100	90
GZ-CuAl10Ni	128	120
EN-GJS-400 (GGC-40)	115	115
EN-GJL-25 (GG-25)	70	70
PA-12 cast	23	23

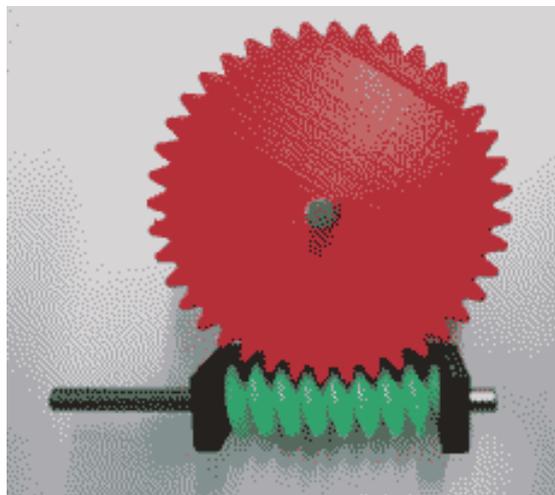
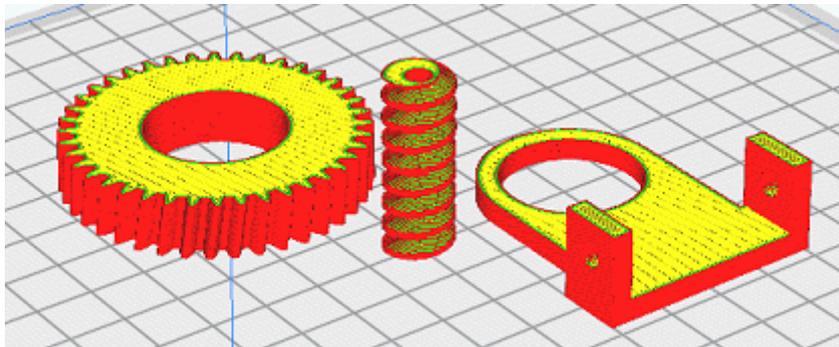
ZAR3+: Tooth contact axial

The meshing of worm and worm wheel can now also be represented in axial section in addition to the radial section. Also 1-tooth worms (ZI) are now displayed.



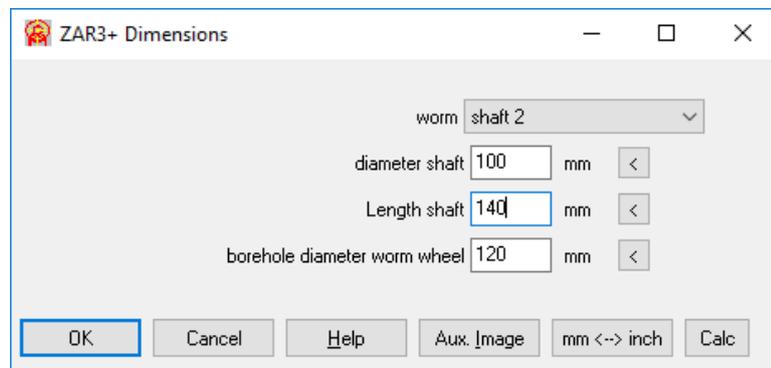
ZAR3 +: Worm gear model with 3D printer

The calculated cylindrical worm can now also be output as STL file and create a model with 3D printer (ZI worm). The associated worm wheel can not be issued as globoide worm wheel, but at least as a helical gear wheel.



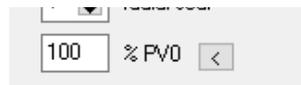
ZAR3 +: bore and shaft for worm and worm wheel

For worm and worm wheel you can enter a bore under "Dimensions 2". For the worm, it can be a shaft rather than a hole. "Shaft 1" is 1 shaft extension on the worm gear (for overhung bearing assembly), and "shaft 2" a shaft on both sides of the worm. The dimensions are used for STL files. When producing a worm with 3D printer, it is better to use only "bore" or "shaft1".



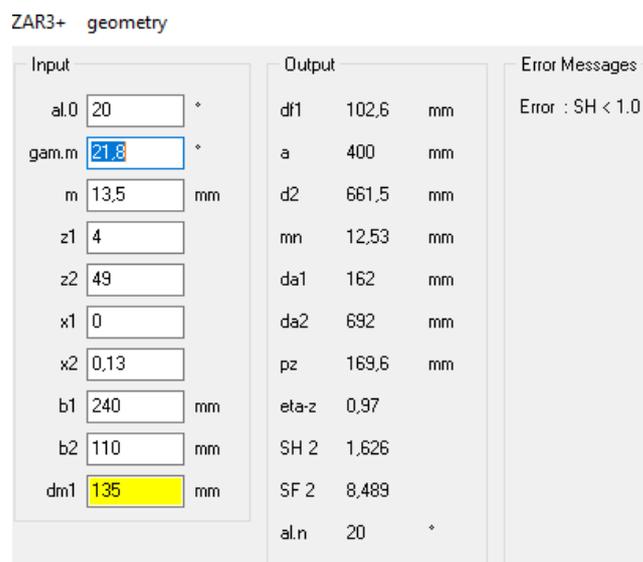
ZAR3 +: factor for no-load power loss PV0

The calculated no-load power loss PV0 sometimes seems too high for small, high-speed worm gears. The calculated no-load power loss at drive speed above 1000 rpm is often higher than the driving power, especially if plastic worm gears are used and therefore the drive power must be much smaller than in steel / bronze gear pairs. Efficiency and output power are then 0, and strength calculation is not possible. In order to be able to continue calculating or to adapt the calculation to measured values, one can now enter a factor for the consideration of the calculated no-load power loss PV0. Default is 100%.



ZAR3 +: Input dm1 for recalculation

The mean pitch diameter is actually a calculated value. If you change dm1, the module has been adjusted so far. The module stays the same now, instead the helix angle gamma_m changes.



ZAR3 +: axial pressure angle of the worm alphax

The axial pressure angle of the worm alphax was incorrectly output (smaller than alphan instead of larger than alphan). This only had an effect on worm gears with ZA profile, because there is alphax = alpha0, and alphan is calculated.

ZAR3 +: Input mx at “Dimensioning” changes either gamma_m or x2

If you enter the module at “Dimensioning”, dm1 and gamma_m are recalculated. If you want integers or standardized dimensions for m as well as for dm1, the profile shift x2 is calculated first. If $-0.5 > x2 < 1.0$, x2 is set, otherwise dm1 and gamma_m are recalculated as before.

ZAR3+: Lubricant database

For entering the lubricant viscosity at 40 ° C and 100 ° C, there is now a small lubricant database as input help.

OIL_NAME	TYPE	V40	V100	INDEX	POUR	FLASH	SOURCE
SHC 150	1	150	22,2	176	-45	233	Mobil Gear
SHC 220	1	220	30,4	180	-39	233	Mobil Gear
SHC 320	1	320	40,6	181	-33	233	Mobil Gear
SHC 460	1	460	54,1	184	-27	234	Mobil Gear
SHC 680	1	680	75,5	192	-27	234	Mobil Gear
SHC 1000	1	1000	99,4	192	-24	234	Mobil Gear
GH 6-32	4	32	7	150	-45	220	Kluebersynth
GH 6-80	4	80	16	200	-35	280	Kluebersynth
GH 6-100	4	100	20	200	-35	280	Kluebersynth
GH 6-150	4	150	28	210	-35	280	Kluebersynth
GH 6-220	4	220	41	220	-30	280	Kluebersynth
GH 6-320	4	320	58	230	-30	280	Kluebersynth
GH 6-460	4	460	79	240	-25	280	Kluebersynth
GH 6-680	4	680	116	260	-25	280	Kluebersynth
GH 6-1000	4	1000	167	260	-25	280	Kluebersynth
GLYG 68	0	68	11,8	170	-30	265	Mobil Glygoyl
GLYG 100	0	100	17,3	190	-30	265	Mobil Glygoyl

ZAR3+: Diagram $a = f(\gamma_m)$

In the worm gear, γ_m is the pitch angle of the worm and the helix angle of the worm wheel. The helix angle changes the center distance, or γ_m (β_2) is calculated for a given center distance.

$$\beta_2 = \gamma_m$$

$$\beta_1 = \Sigma - \beta_2 = 90^\circ - \beta_2 = 90^\circ - \gamma_m$$

$$a_0 = \frac{m_n}{2} * (z_1 / \cos(\Sigma - \beta_2) + z_2 / \cos(\beta_2))$$

The function can now be represented as a diagram $a = f(\gamma_m)$, either for " $m_n = \text{const}$ " or " $m_x = \text{const}$ ".

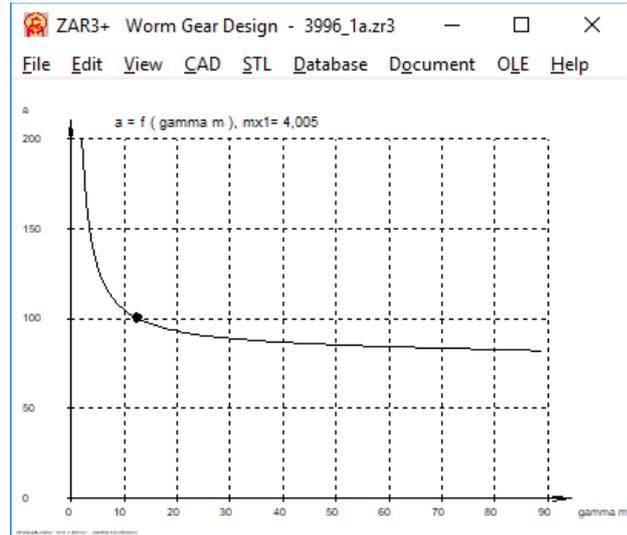
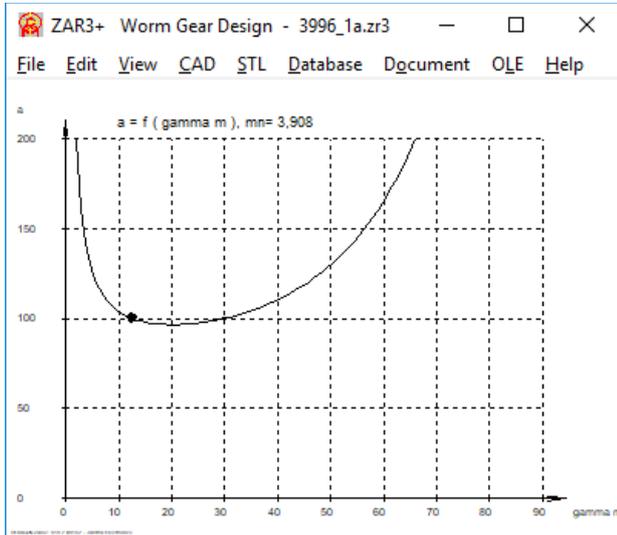
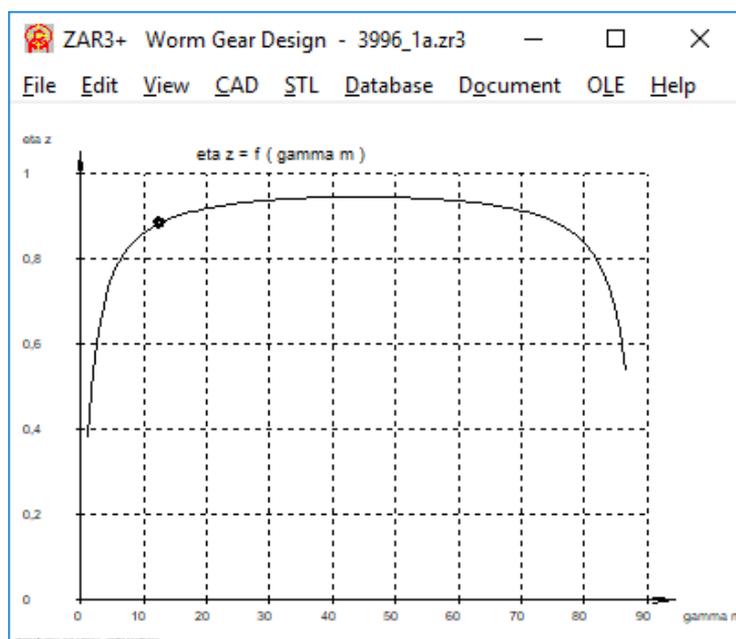


Diagram shows the smallest possible center distance, if m_n remains constant. With worm gears, however, the axial modulus of the worm is normally specified, which corresponds to the tangential modulus of the worm wheel at 90° crossing angle ($m_{x1} = m_{t2}$). Then $m_n = m_{t2} * \cos(\beta_2)$ and $a_0 = m_{x1} / 2 * \cos(\beta_2) * (z_1 / \cos(\Sigma - \beta_2) + z_2 / \cos(\beta_2))$

ZAR3+ Diagram $\eta_z = f(\gamma_m)$

The efficiency is also dependent on the helix angle. However, you can not increase the helix angle arbitrarily, otherwise the core diameter of the worm goes to zero.

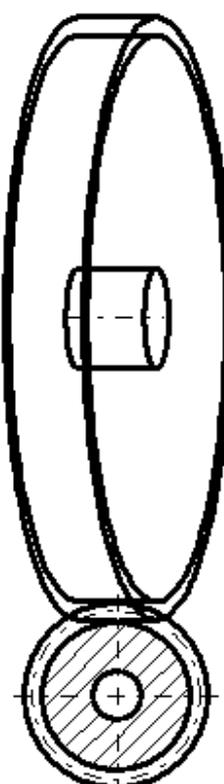


ZAR9: software for cross-helical gear design

ZAR9 cross-helical gear design - dec244.zr9

File Edit View CAD STL Database Document OLE Help

Decker Maschinenelemente Aufgaben 2011
24.4
Schraubrad 1, Schraubrad 2



Dimensions		
mn	mm	4,000
a	mm	188,89
alpha	°	20,00
summa	°	76,00

Dimensions		
z		16
beta	mm	41,000
beta b	mm	38,061
d	mm	84,801
da	mm	92,801
df	mm	74,801
db	mm	76,382
b	mm	40,00
x		0,0000
alpha t	mm	25,746

power		
PN	kW	0,823
TN	Nm	20,96
n	/min	375
FN	N	618

material		
material	Worm	Worm wheel
E	MPa	206000
SigHlim	MPa	1500
SigFE	MPa	800

safety		
SV (Sig.HV= 1500)		2,33
SS		1,47
SF		8,54

tool		
hfP0/mm	1,00	1,00
haP0/mm	1,25	1,25
raP0/mm	0,25	0,25
rP0/mm	0,00	0,00

u		
eps.n		1,785
KA		1,250
vg m/s		2,0
pr1		19,15

gear 1 (worm) 1		
mn	mm	4,000
mr	mm	5,300
mx	mm	6,097
z		16
alpha n	°	20,00
beta	°	41,00
tooth alignment		right hand
da	mm	92,801 ± 0,000
d	mm	84,801
db	mm	76,382
df	mm	74,801 ± 0,000
pn	mm	12,566
sn	mm	6,283 ± 0,000
ha	mm	4,000
hf	mm	5,000
h	mm	9,000
xe		0,000 ± 0,000
MaK (d=10,4)	mm	98,984 ± 0,000
a	mm	188,893
summa	°	76,000

gear (helical) 2		
mn	mm	4,000
mr	mm	4,883
mx	mm	6,974
z		60
alpha n	°	20,00
beta	°	35,00
tooth alignment		right hand
da	mm	300,986 ± 0,000
d	mm	292,986
db	mm	267,746
df	mm	282,986 ± 0,000
pn	mm	12,566
sn	mm	6,283 ± 0,000
ha	mm	4,000
hf	mm	5,000
h	mm	9,000
xe		0,000 ± 0,000
MaK (d=10,4)	mm	315,401 ± 0,000
a	mm	188,893
summa	°	76,000

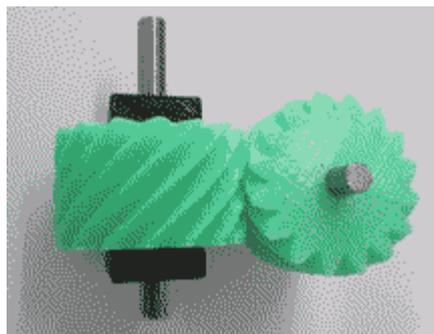
efficiency		
mu z		0,105
eta z		0,849
PVz	kW	0,124
PV0 (25%)		0,013
PVLP	kW	0,008
PVD	kW	0,000
PV	kW	0,138
eta		0,823

Force		
Ft	N	618
Fx	N	433
Fy	N	265
Fz	N	799

Soon we can provide a new software for cross-helical gear design. The dimensions of cross-helical gears are calculated similarly to worm gears, so that most dimensions for 90° axis angles can also be calculated with ZAR3+. Instead of a line contact like a globoid worm wheel, there is only one point touch on the cross-helical gear. Therefore, in the cross-helical gear compared with a worm gear of the same dimensions, the load capacity is worse and the efficiency similarly poor.

Incidentally, ZAR3+ can also be used to calculate a worm gear that is more similar to a pair of cross-helical gears: enter the same number of teeth z_1 and z_2 and $\gamma_m = 45^\circ$, results in the same dimensions of worm and worm wheel. When created with a 3D printer, the worm and worm wheel (as a helical wheel, not as a globoid wheel) are exactly the same.

There are several types of cross-helical gears: worm and helical gear with 90° axis angle as worm gear replacement, two cross-helical gear wheels with 90° axis angle, or the same with an axis angle between 30° and 90° .



ZAR1+, ZAR3+,ZAR5,67,8,ZARXP, ZAR1W: Settings: z slice

Helical gears and worm gears are shown in layers. The layer thickness can now be configured under File \ Settings \ CAD. We suggest to configure the default layer thickness of your 3D printer as z_slice. Attention: If you reduce the layer thickness so that the STL model is displayed with smaller steps, the size of the STL file increases accordingly. In any case, the STL file of helical gears will be many times larger than that of spur gears. Helical gears and worms from the 3D printer can only be used to a limited extent, depending on the layer thickness, the slope is a step function with larger or smaller steps and corresponding unevenness. File \ Settings \ CAD:



ZAR1W, ZAR1+: xe tolerance

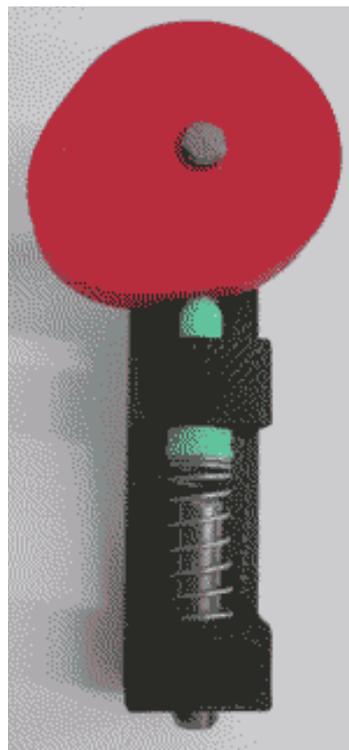
The +/- tolerance of the generating profile shift factor x_e had been displayed too large in the gear table. Since tolerance +/- from the mean value, half the value for the tolerance applies.

SR1 / SR1 +: Less warnings for missing database data for temperature dependency

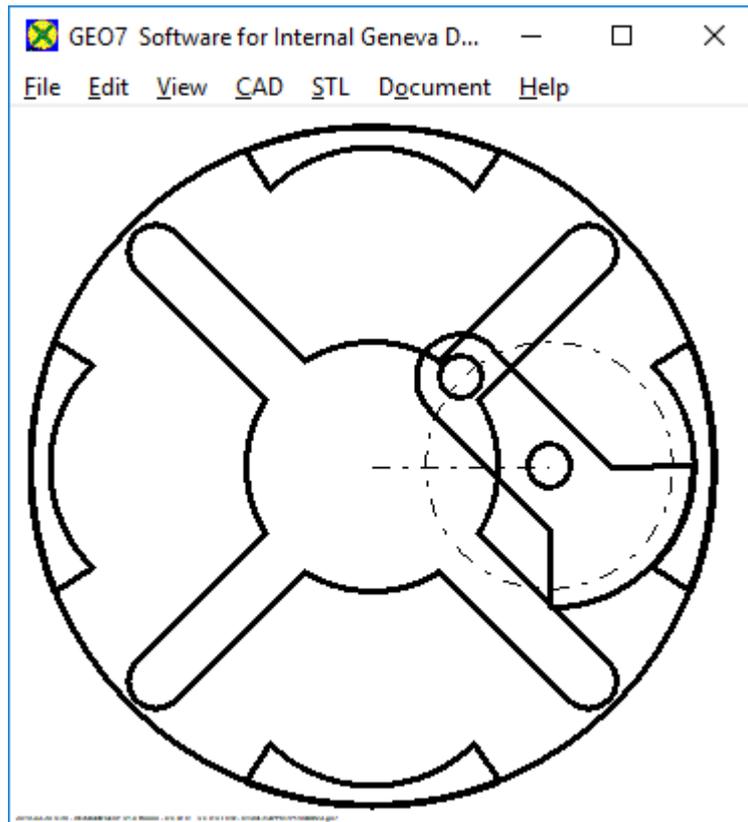
When you enter a working temperature, you sometimes get warnings like "mat_p_re.dbf: material name?". This means that there are no material data for the temperature dependence of yield strength and Young's modulus. There are fields in the database for the values at 100 .. 700 ° C. If the entered working temperature is less than 100 ° C, these warnings will no longer appear in the future because at 100 ° C modulus of elasticity and yield strength change only slightly. The most important influencing factor is anyway the temperature expansion coefficient α_T , and this one is known for all materials.

GEO4: create model with 3D printer

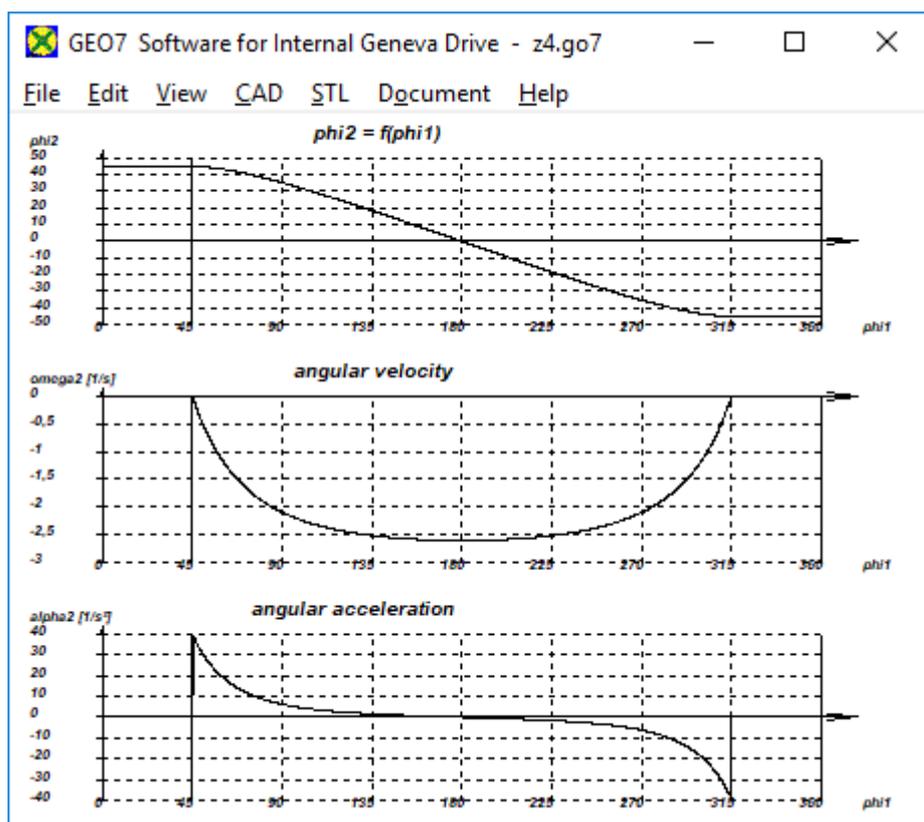
In addition to cams or cam discs, you can now also create plungers and a carrier plate as STL file and produce with 3D printer.



GEO7: Software for Internal Geneva Gears

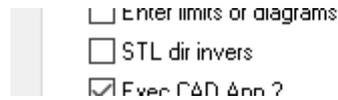


GEO7 calculates stepper gear with internal Geneva wheel. Interior Maltese have a long switching time and a short rest time compared to external Maltese gears. In a 4-beam external Geneva gear, the switching angle is 90° and the locking angle is 270° . In case of an internal Geneva drive, the reverse is true: switching angle 270° and locking angle 90° .



Reverse STL direction

Under "File \ Settings \ CAD" (STL Dir invers) you can now reverse the direction of the STL-3D objects if your program to open the STL files displays the 3D object in the wrong color or reports the wrong direction.



Change Licensee name: 40 Euro

The name of the licensee is fixed in the program and can not be changed by you. For updates, the name of the licensee usually remains unchanged. If you want to change your company name in the program as part of an update, because the name has changed or the company was merged or acquired, please order the name change for a fee of 40 Euros (plus the update price). Otherwise, the name of the licensee will remain unchanged in the new version. Maximum 30 characters are possible.

Key code problem with Windows 10 or network version

If you always need new key codes for your network version if the server or volume has been replaced or volume settings modified, but the path remained the same, you can update to a version with permanent key code, but your program path must also remain permanent. When updating, please specify the network path (UNC path, no logical drive), e.g. \\ourserver659\HEXAGON\, then you get an update with permanent code that does not change anymore (if the path does not change). Then you need new key codes for the last time. License agreement then please also update with UNC path and copy back as a pdf file.

A similar problem exists for single-user licenses under Windows 10. For large Windows updates, Windows reduces the usable size of the hard disk in favor of an invisible Microsoft partition. The only solution is to install the software not on the system partition C:, but on another partition or hard disk. If your PC has an SSD disk and a large hard disk, do not install HEXAGON software on the SSD if Windows is installed there. Better install it on the large disk. Another option is to install HEXAGON software on an external hard drive. Then HEXAGON software remains on the external hard drive, even if computer changes, without needing new key codes.

Did you know ? Show database sorted

NAME1	NAME2	NAME3	NAME4	G	E	DICHTe	RMO
Titan Grade 5 ST+age	spring temper	Ti-6Al-4V, ST	3.7165	44000	114000	4,42	
Titanium Grade 5	annealed	Ti-6Al-4V, annealed	3.7165	44000	114000	4,42	
Titanium Grade 1	Ti99	3.7025	ASTM B348	40000	110000	4,5	
Ti 3-8-6-4-4, ST+age	AMS 4957 Beta-C	Ti-3Al8V6Cr4Mo4Zr	solution treat.+aged	39000	99000	4,82	
EN 10270-3-1.4462-S2	X2CrNiMoN22-5-3	Sandvik Springflex	UNS S322205/S31803	79000	205000	7,8	
EN 10270-3-1.4462-S3	X2CrNiMoN22-5-3	Sandvik SpringflexSH	UNS S322205/S31803	79000	205000	7,8	
Roeslau-Extra	High Carbon Wire	Music Wire		82000	206000	7,8	
Roeslau-Extra-Extra	High Carbon Wire High-Tens.	Music Wire		82000	206000	7,8	

All databases can be sorted by any column by clicking with the right mouse button in the title field (here "DENSITY" or "DICHTe")

HEXAGON PRICE LIST 2019-05-01

PRODUCT	EUR
DI1 Version 1.2 O-Ring Seal Software	190.-
DXF-Manager Version 9.1	383.-
DXFPLOT V 3.2	123.-
FED1+ V30.9 Helical Compression Springs incl. spring database, animation, relax., 3D,..	695.-
FED2+ V21.3 Helical Extension Springs incl. Spring database, animation, relaxation, ...	675.-
FED3+ V21.1 Helical Torsion Springs incl. prod.drawing, animation, 3D, rectang.wire, ...	600.-
FED4 Version 7.7 Disk Springs	430.-
FED5 Version 16.2 Conical Compression Springs	741.-
FED6 Version 16.8 Nonlinear Cylindrical Compression Springs	634.-
FED7 Version 13.8 Nonlinear Compression Springs	660.-
FED8 Version 7.2 Torsion Bar	317.-
FED9 Version 6.3 Spiral Spring	394.-
FED10 Version 4.3 Leaf Spring	500.-
FED11 Version 3.5 Spring Lock and Bushing	210.-
FED12 Version 2.6 Elastomer Compression Spring	220.-
FED13 Version 4.2 Wave Spring Washers	228.-
FED14 Version 2.2 Helical Wave Spring	395.-
FED15 Version 1.6 Leaf Spring (simple)	180.-
FED16 Version 1.3 Constant Force Spring	225.-
FED17 Version 1.9 Magazine Spring	725.-
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